

Continuation in Experiments

Lecture given during
Advanced Summer School on
Continuation Methods for Nonlinear Problems

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Outline

- ▶ basic idea
- ▶ experiments (mechanical)
- ▶ simulations (random dynamic network problem)

Experimental results

- ▶ (forced mechanical oscillators) DAW Barton (Univ. Bristol)
- ▶ (forced mechanical oscillators) DTU group (J Starke, F Schilder, E Bureau, JJ Thomsen, I Santos)
- ▶ (static bucking) Neville et al. (Bristol)

General terms and conditions

To do (in experiments)

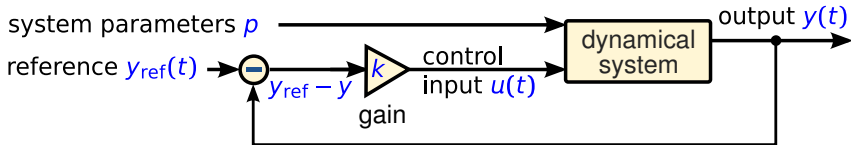
- ▶ Continue equilibria & periodic orbits that are either
 - ▶ dynamically unstable or
 - ▶ depend sensitively on system parameters

Constraints

- ▶ no setting of internal state possible
- ▶ accuracy independent of model
- ▶ good estimate for error
- ▶ avoid system identification
- ▶ no real-time computations

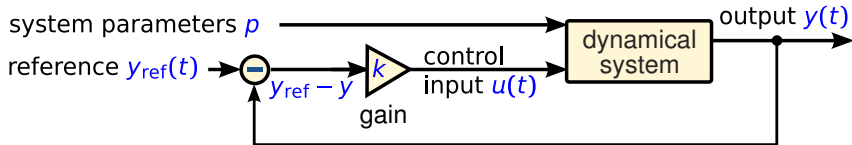
Basic idea

Feedback control



Basic idea

Feedback control

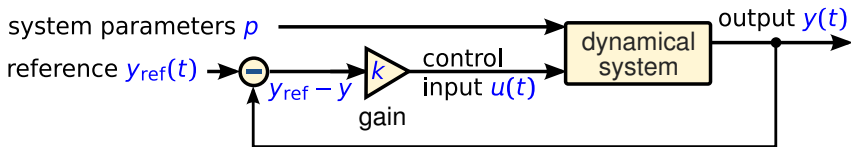


Classical control engineering

- reference $y_{\text{ref}}(t)$ given
 - make output y track $y_{\text{ref}}(t)$
- ⇒ (e.g.) integral components in “ k ”
- Questions: stability, optimality, robustness,...

Basic idea

Feedback control



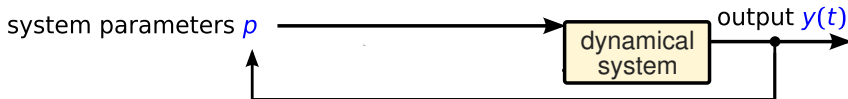
Find equilibria

$$\frac{d}{dt}y_{\text{ref}} = k_w[y - y_{\text{ref}}]$$

- washout filter (Abed *et al* 2004)
- ⇒ equilibria with control = equilibria without control
- suppresses Hopf, period doubling

Basic idea

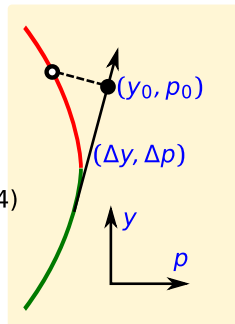
Feedback control



Find equilibria

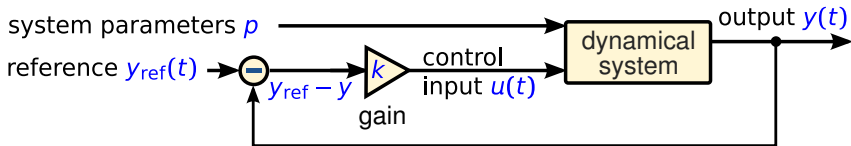
$$\frac{d}{dt}q = \Delta y^T(y - y_0) + \Delta p(p - p_0)$$
$$p = p_{\text{ref}} + [k_y, k_p] \begin{bmatrix} y - y_0 \\ q \end{bmatrix}$$

- control through parameter p (Siettos *et al* 2004)
- ⇒ continuation around saddle-node
- for Poincaré map by Misra *et al* 2008



Basic idea

Feedback control

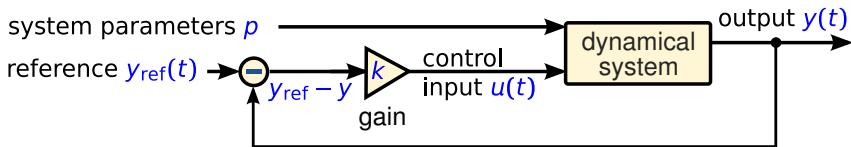


Find periodic orbits

- Time-delayed feedback (Pyragas): $y_{\text{ref}} = y(t - T)$
- Extended (Gauthier): $y_{\text{ref}} = (1 - \varepsilon)y_{\text{ref}}(t - T) + \varepsilon y(t - T)$
- T period, $0 < \varepsilon \leq 1 \Rightarrow$ system with delay
- periodic orbits of period T with control = periodic orbits of period T without control
- stabilizing gains $k(t)$ exist for single input

Basic idea

Feedback control



General approach

- k stabilizing $\Rightarrow y(t) \rightarrow y_{\infty}(t; y_{\text{ref}}, p)$ for $t \rightarrow \infty$
- **Input-Output Map:** $(y_{\text{ref}}, p) \mapsto y_{\infty}$
- **Solve** (e.g. Newton iteration)

$$y_{\text{ref}} = y_{\infty}(y_{\text{ref}}, p)$$

for y_{ref} and p in $\mathbb{R}^n$ or function space
(few Fourier modes for y_{ref})

- $u \rightarrow 0$ for $t \rightarrow \infty$ in solution
- branch points equal branch points of uncontrolled system

Controlled experiment = fixed point map

- ▶ assume experiment with controllable equilibrium y_* (location unknown), and stabilising feedback

$$u(t) = k^T [y_{\text{ref}} - y(t)]$$

⇒ this defines **nonlinear input output map**

- ▶ $y_{\infty} : (y_{\text{ref}}, p) \mapsto \lim_{t \rightarrow \infty} y(t)$
- ▶ One evaluation of y_{∞} :
 1. set system parameters to p ,
 2. set input to feedback law to $u(t) = k^T [y_{\text{ref}} - y(t)]$ (y is state/output)
 3. Wait until transients have settled: $y_{\infty}(y_{\text{ref}}, p) := \lim_{t \rightarrow \infty} y(t)$
- ▶ y_{ref} is equilibrium of uncontrolled experiment if and only if

$$y_{\infty}(y_{\text{ref}}, p) = y_{\text{ref}} \quad (\text{which implies } \lim_{t \rightarrow \infty} u(t) = 0)$$

Controlled experiment = fixed point map

- ▶ For **periodic orbit** $y_*(t)$ and stabilising feedback

$$u(t) = k^T[y_{\text{ref}}(Tt) - y(t)]$$

⇒ **nonlinear input output map** with $[0, 1]$ -**periodic** y_{ref}

- ▶ $y_{\infty} : (y_{\text{ref}}(T\cdot), T, p) \mapsto \lim_{n \rightarrow \infty} y(nT + T\cdot)$
- ▶ One evaluation of y_{∞} :
 1. set system parameters to p ,
 2. set input to feedback law to $u(t) = k^T[y_{\text{ref}}(t) - y(t)]$
 3. Wait until transients have settled:
 $y_{\infty}(y_{\text{ref}}, T, p)(s) := \lim_{n \rightarrow \infty} y(nT + Ts)$
- ▶ y_{ref} is **periodic orbit** of uncontrolled experiment if and only if

$$y_{\infty}(y_{\text{ref}}, T, p) = y_{\text{ref}} \quad (\text{which implies } \lim_{t \rightarrow \infty} u(t) = 0)$$

- ▶ **impose phase condition**, pseudoarclength condition on y_{ref}, T, p
- ▶ (e.g.) **represent** y_{ref} **by its first Fourier modes**

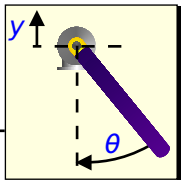
Periodically forced example: rotation in pendulum

Schema

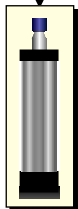
excitation $p \sin(\omega t)$

angle $\theta(t)$

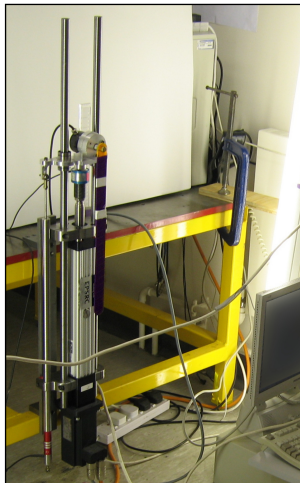
encoder



actuator



$y(t)$



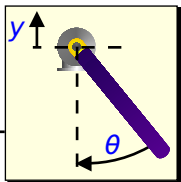
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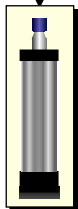
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pendulum

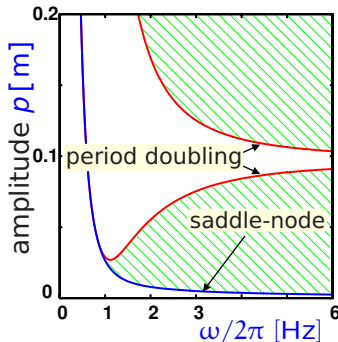
actuator



$y(t)$

Numerics

rotation



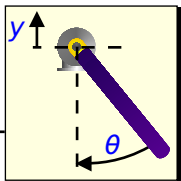
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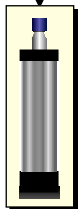
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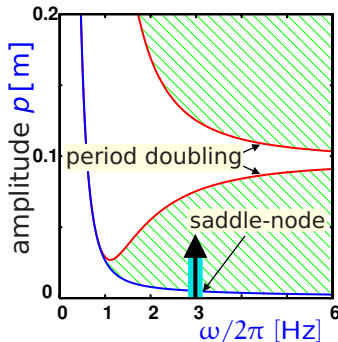
actuator



$y(t)$

Numerics

rotation



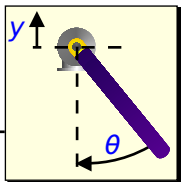
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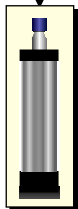
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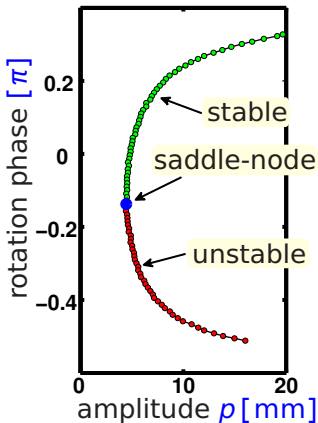
actuator



$y(t)$

Experiment

rotation



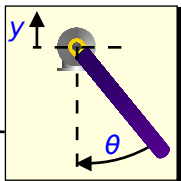
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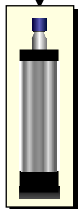
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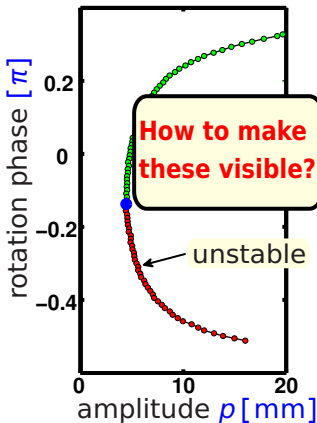
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$y(t)$

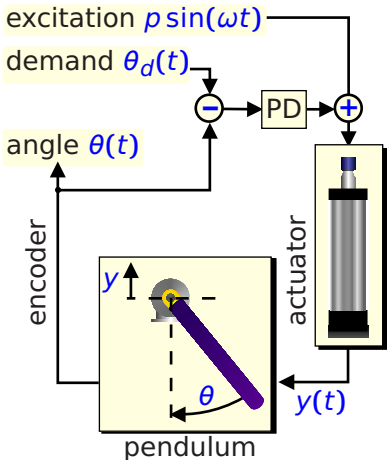
Experiment

rotation



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Schema



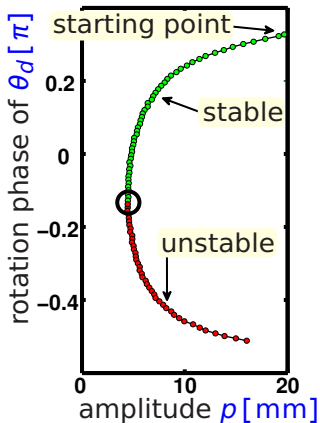
Control

- feed back $\theta - \theta_d$
 $\Rightarrow$ always stable
 $\Rightarrow$ output not natural
- How to choose θ_d ?
 $\Rightarrow$ find θ_d
such that $\theta_d - \theta = 0$

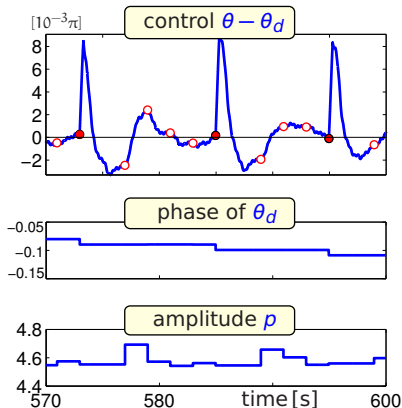
Experimental results

Experiment

bifurcation diagram



time profile of continuation



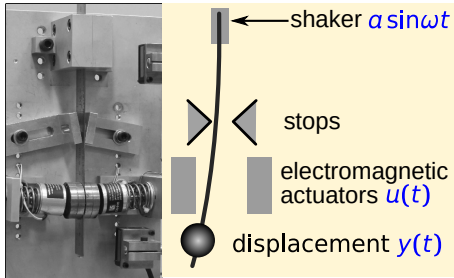
Experimental results

video

Mechanical experiments (periodically forced)

Backlash/impact oscillator (Results from Bureau *et al*, 2014)

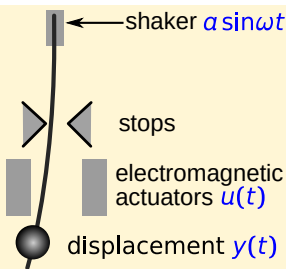
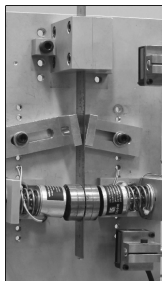
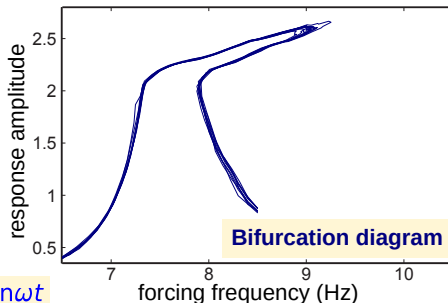
- CONTINEX (COCO)
numerical continuation
toolbox by F Schilder
- discretization of y_{ref} :
5 Fourier modes



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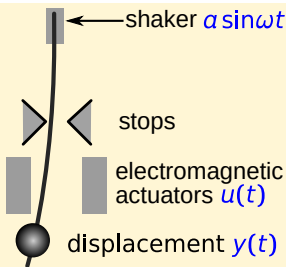
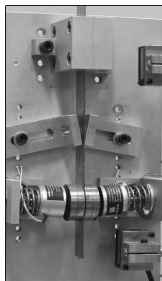
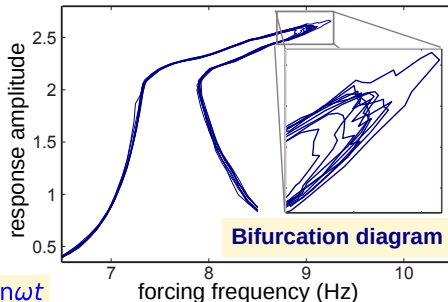
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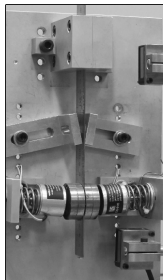
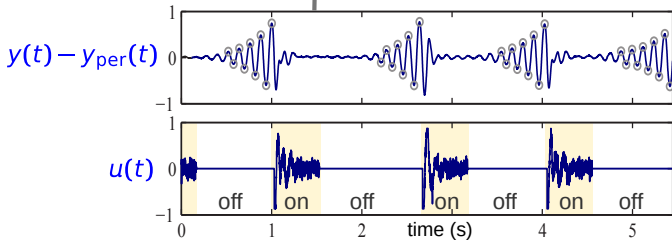
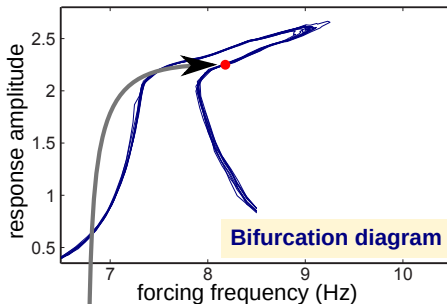
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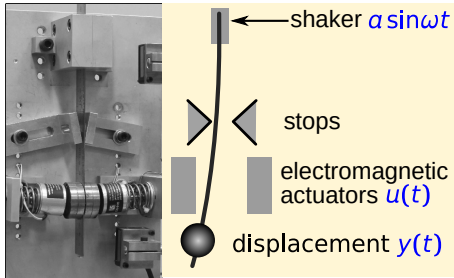
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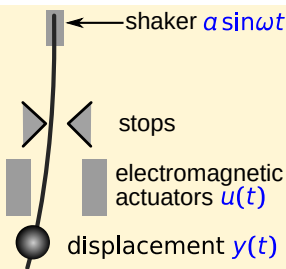
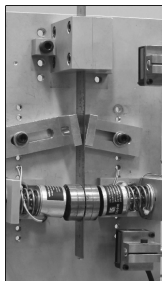
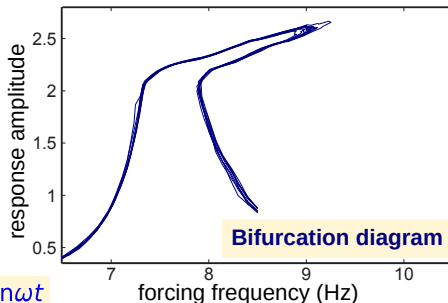
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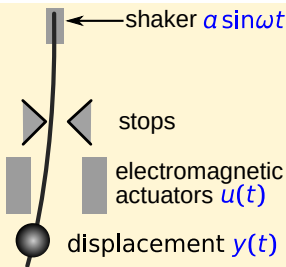
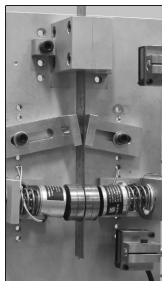
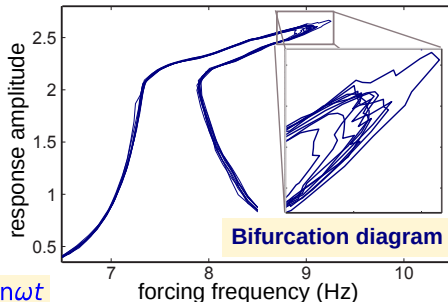
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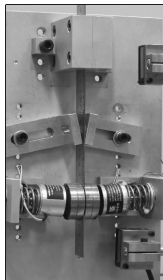
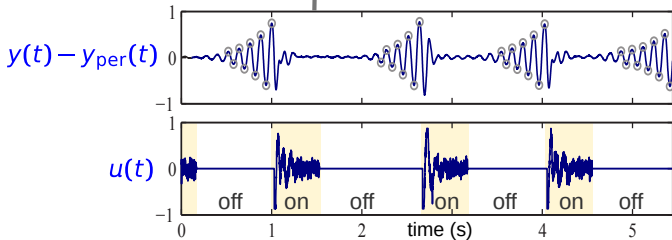
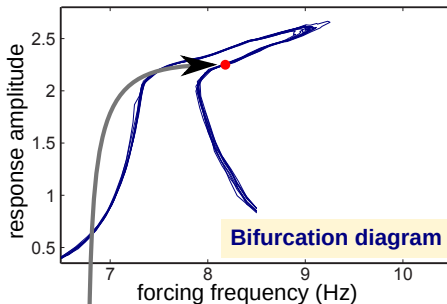
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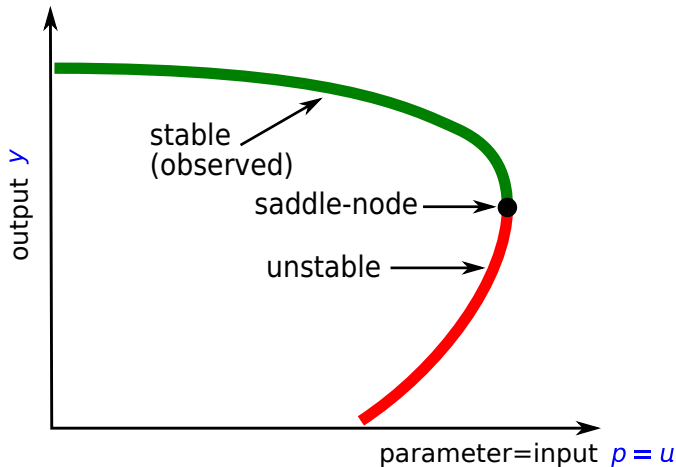
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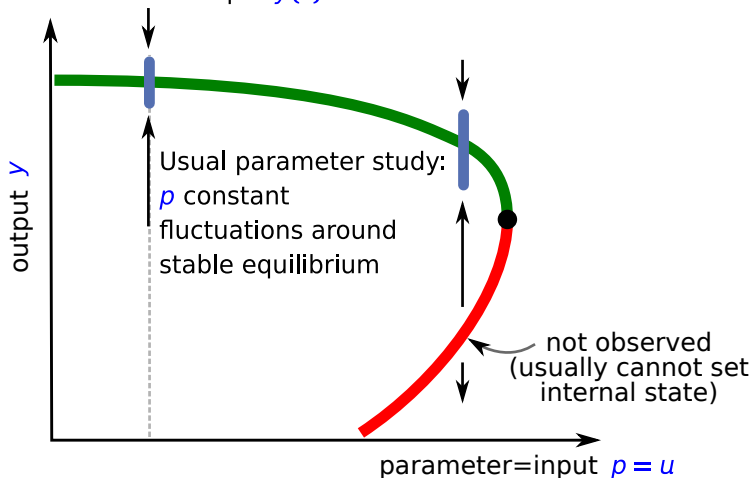
Simplification of *Siettos et al* (2004)

input $u(t)$ is bifurcation parameter p
output $y(t)$



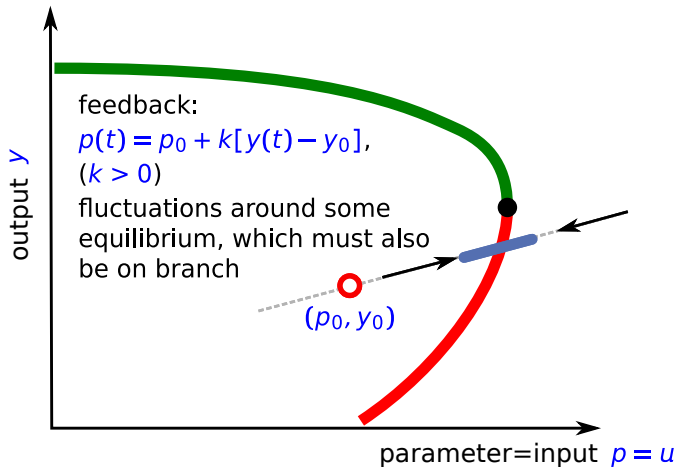
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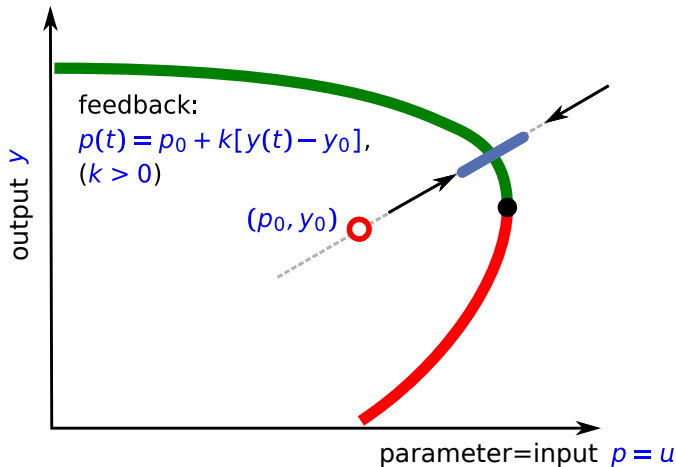
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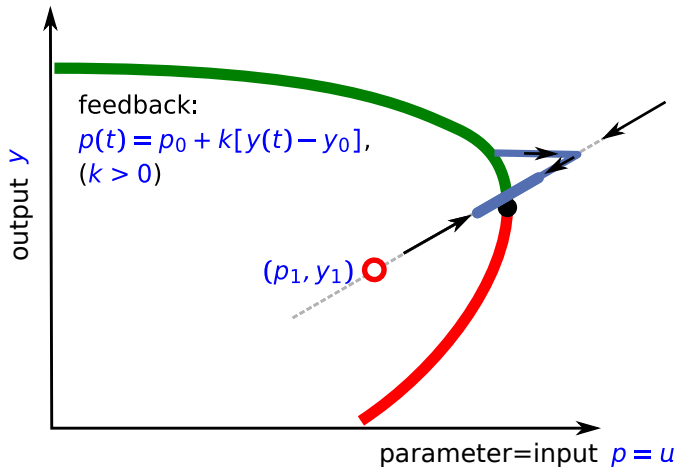
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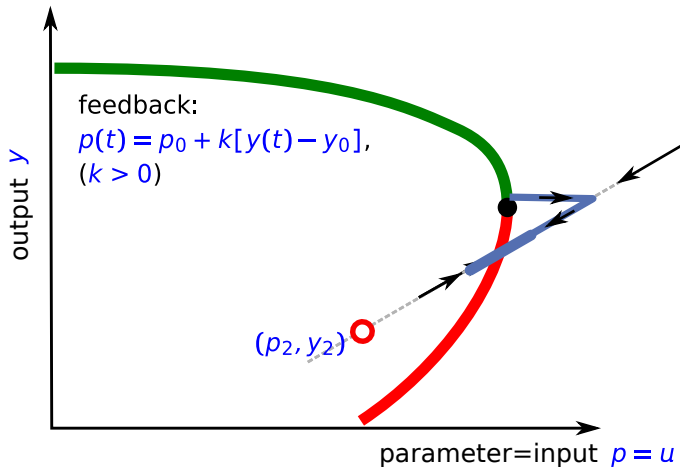
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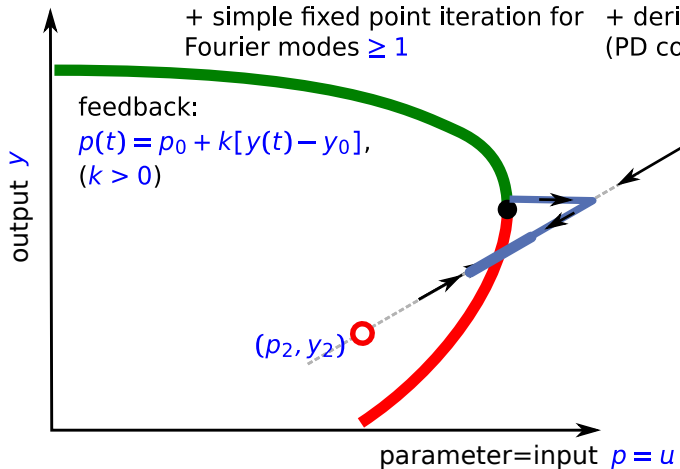
Simplification of *Siettos et al* (2004)

input $u(t)$ is bifurcation parameter p

output $y(t)$

+ simple fixed point iteration for
Fourier modes ≥ 1

+ derivative gain
(PD control)



Motivating example IV

Check for saddle-node normal form:

$$\dot{y} = -p - y^2$$

⇒ Equilibrium $y_s = \sqrt{-p}$ stable, $y_u = -\sqrt{-p}$ unstable.

$$p(t) = p_0 + k[y(t) - y_0]$$

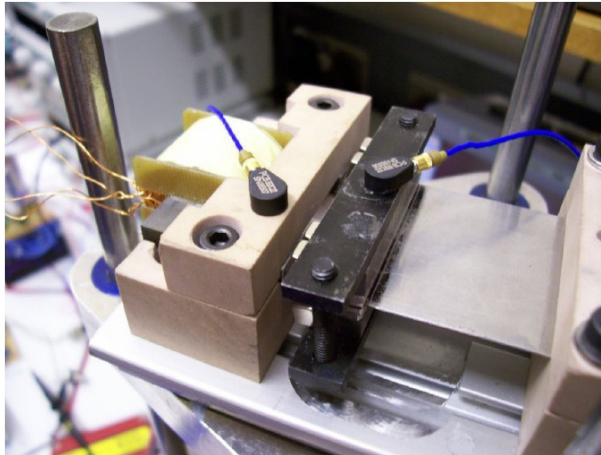
Equilibria satisfy

$$\begin{aligned} 0 &= -p_{\text{eq}} - y_{\text{eq}}^2 \\ &= -\{p_0 + k[y_{\text{eq}} - y_0]\} - y_{\text{eq}}^2 \end{aligned}$$

Stability: $-k - 2y_{\text{eq}}$ ⇒ stable for $y_{\text{eq}} \geq -k/2$.

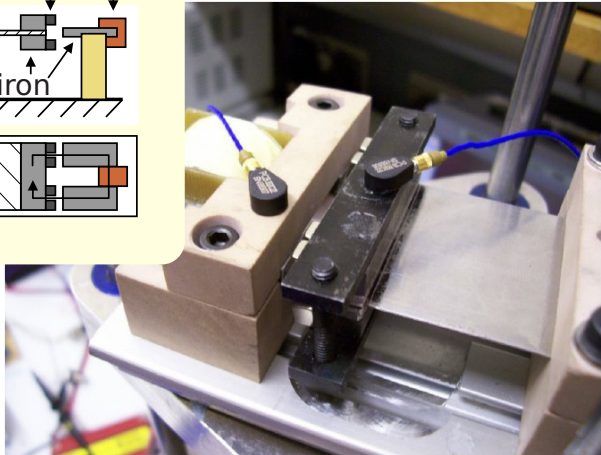
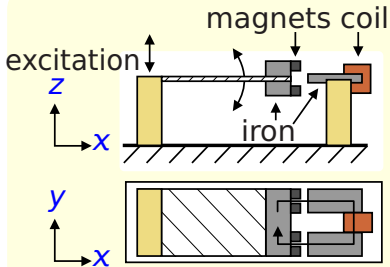
Energy harvester — *Barton & S, 2013*

nonlinear oscillator (damping difficult to model)

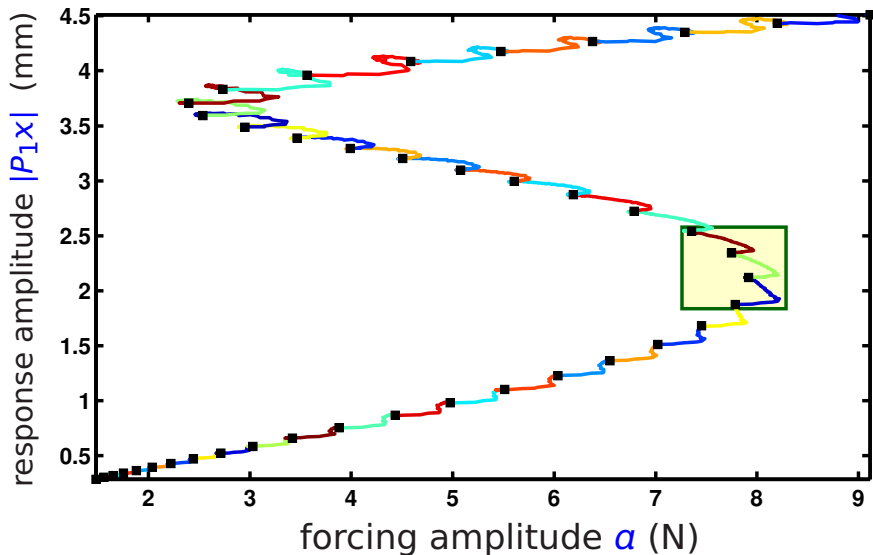


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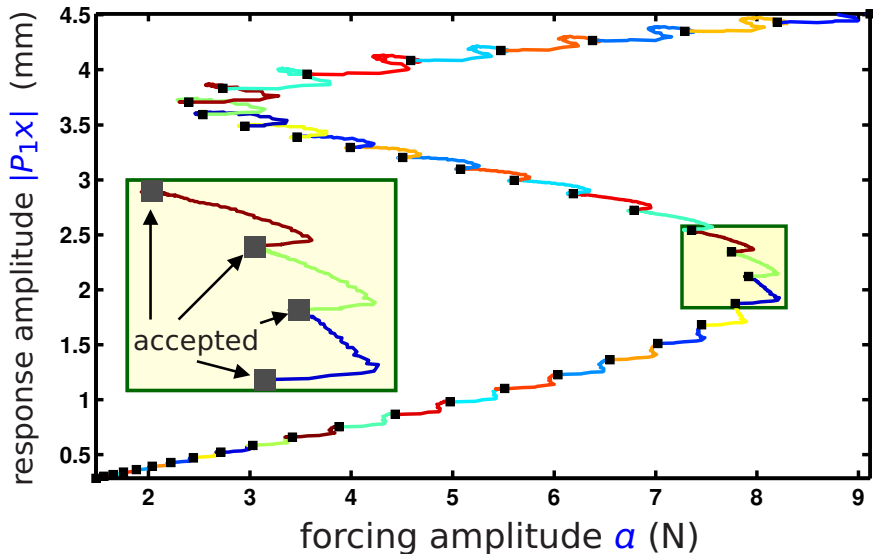
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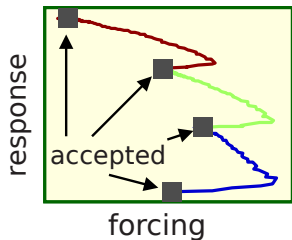
Evolution of control through bifurcation diagram



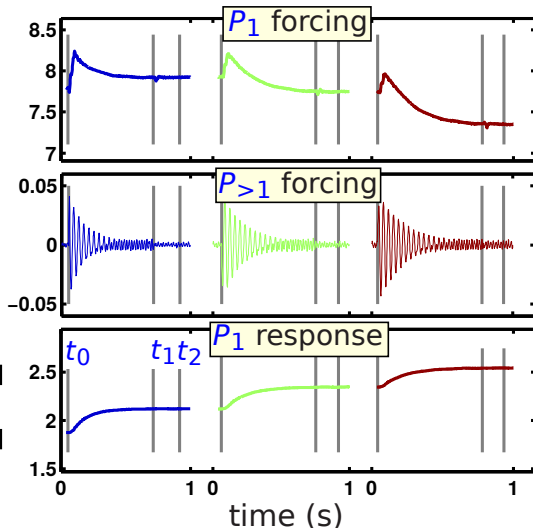
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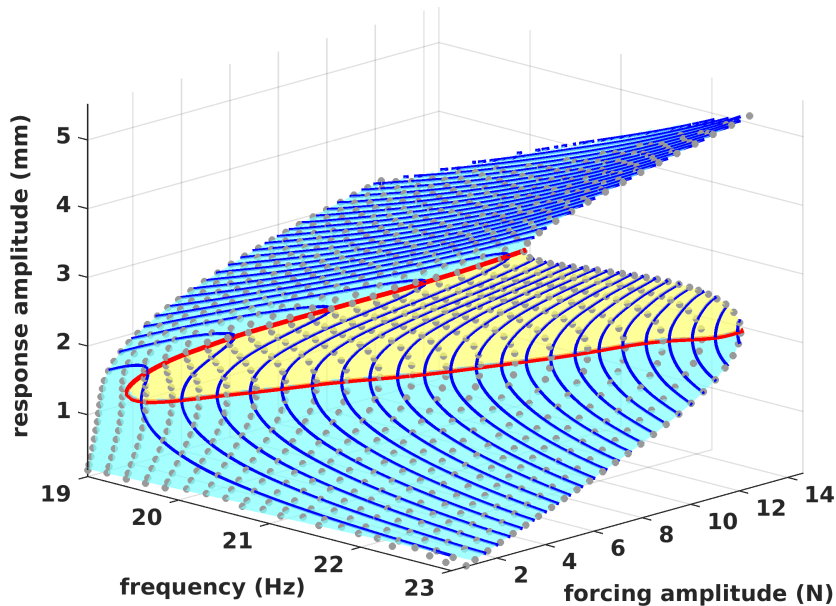
Time profiles



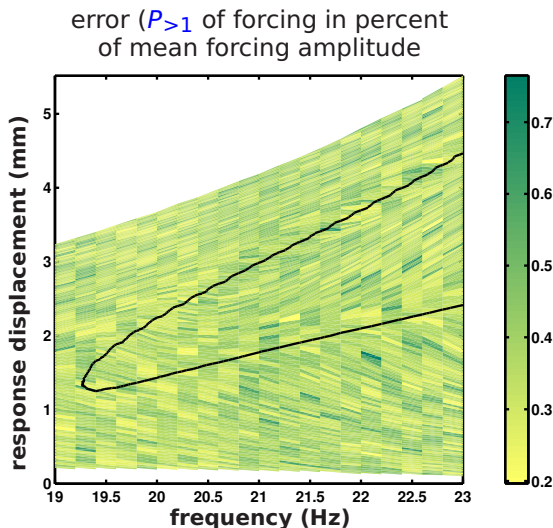
t_0 set new reference
 t_1 control has settled
 $\Rightarrow$ iterate reference
 t_2 control has settled



Solution surface and errors



Solution surface and errors



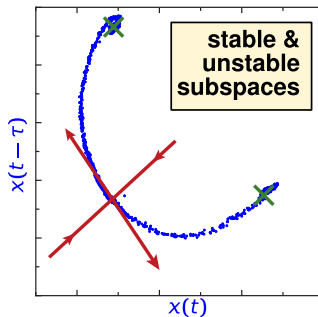
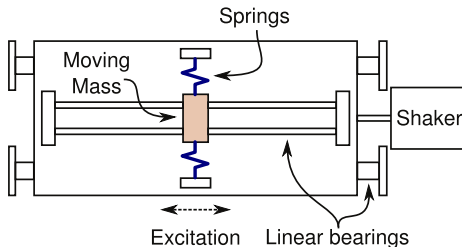
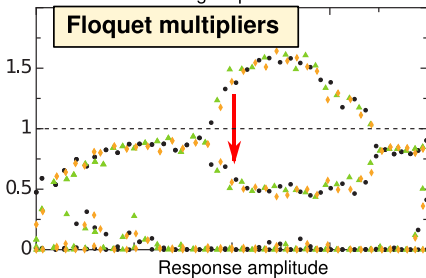
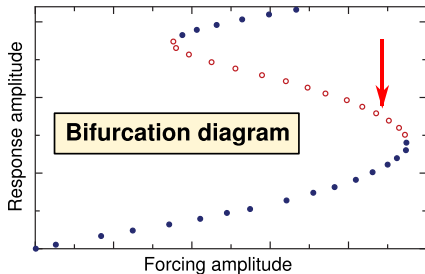
main source of error

derivative component of PD control
(greatly reduced with filtering)

Stable and unstable subspaces of periodic orbits

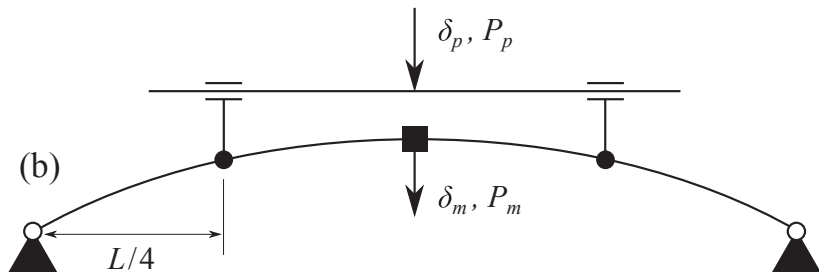
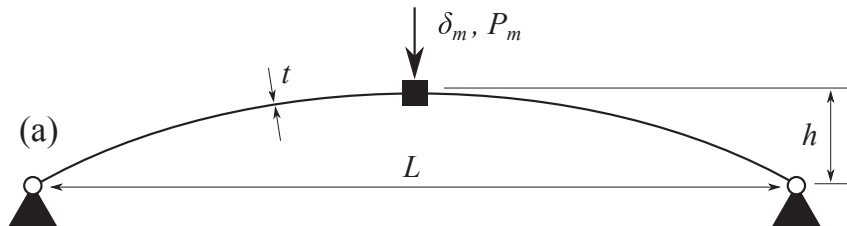
DAW Barton'17

arxiv:1506.04052



Recent experiments on buckling beams

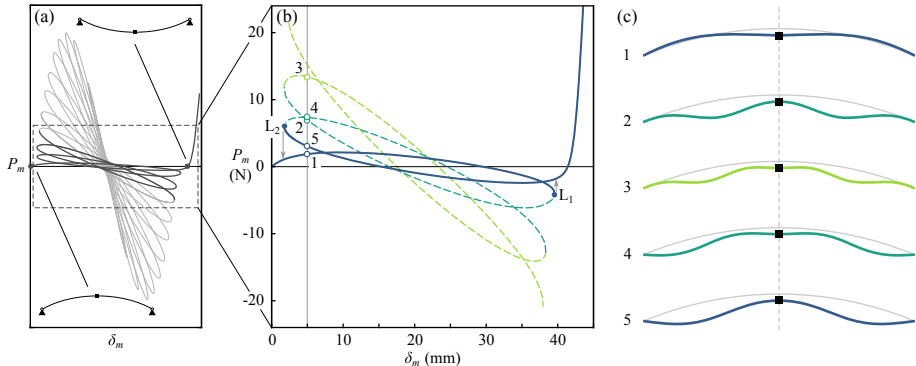
Neville, Groh, Pirrera, Schenk, PRL'18



Recent experiments on buckling beams

Neville, Groh, Pirrera, Schenk, PRL'18

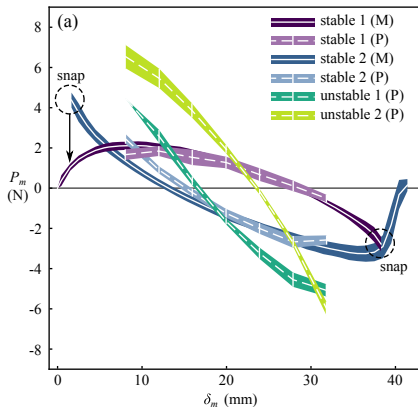
Numerical results for model



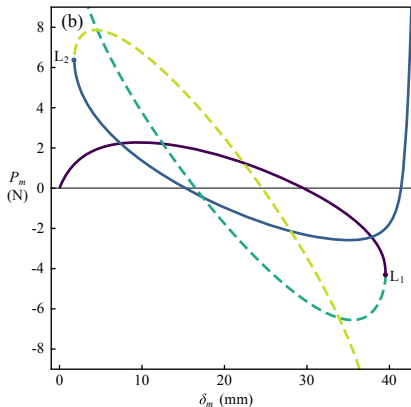
Recent experiments on buckling beams

Neville, Groh, Pirrera, Schenk, PRL'18

Experiment



Model



Using control-based continuation in simulations

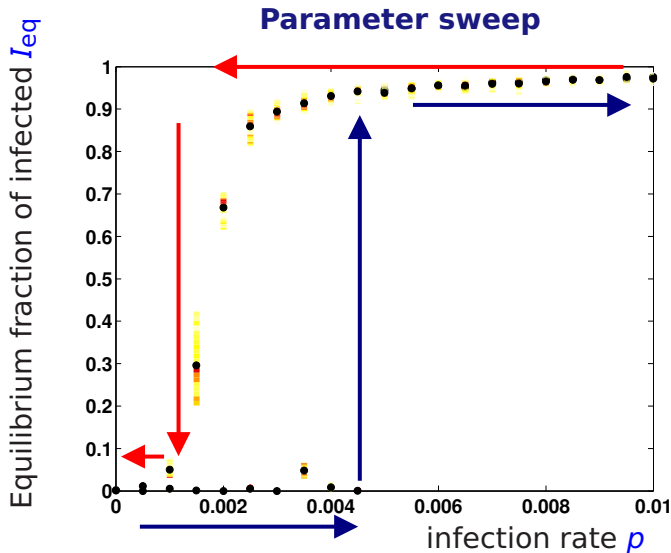
Disease spreading on network

[Gross *et al*, PRL 2006]

- ▶ network with N nodes (individuals) with state either S (susceptible) or I (infected)
- ▶ kN links (initially random, $k \sim 10$)
- ▶ at every step:
 - ▶ I individual recovers with probability r
 - ▶ infection travels along SI link (infects S node) with probability p
 - ▶ SI link is rewired (keep S node, replace I node by random other S node) with probability w
- ▶ system has parameter range where disease-free and endemic equilibrium coexist

Disease spreading on network

[Gross *et al*, PRL 2006]



Disease spreading on network

[Gross *et al*, PRL 2006]

Mean field model

- ▶ I number of infected,
- ▶ L_{ab} number of links between a and b
- ▶ p infection probability, r recovery probability, w rewiring probability

$$\dot{I} = pL_{SI} - rI$$

$$\dot{L}_{II} = pL_{ISI} + pL_{SI} - 2rL_{II}$$

$$\dot{L}_{SS} = (r + w)L_{SI} - 2pL_{SSI}$$

$$N = I + S$$

$$kN = L_{II} + L_{SS} + L_{SI}$$

$$L_{abc} \approx L_{ab}L_{bc}/b \quad \leftarrow \text{closure assumption}$$

Rigorous definition of equilibrium?

- ▶ almost surely disease goes extinct eventually
- ▶ avoid this effect by re-introducing infected nodes
- ▶ for p in bistable regime stochastic system has stationary density with (in projection) 2 well-separated local maxima **stable equilibria**:
 - ▶ disease close to extinct
 - ▶ large number of infected
- ▶ Consider macroscopic output, e.g., I , conditional balance in the long run

$$I_{\text{eq}} = \lim_{t \rightarrow \infty} \text{mean} \{I(s) : s \in [t, t + T], I(s) \in [I_{\text{low}}, I_{\text{up}}]\}$$

(expectation of conditional stationary density)

Proposed definition of (unstable) equilibrium

Include feedback loop:

- ▶ Choose reference fraction of infected I_{ref}
- ▶ at every step:
 - if $I < I_{\text{ref}}$, infect $I_{\text{ref}} - I$ individuals
 - if $I > I_{\text{ref}}$, “cure” $I - I_{\text{ref}}$ individuals
- ▶ I_{ref} is equilibrium value if, after transients have settled
mean artificially cured = mean artificially infected
- ▶ Or: long-time mean of feedback loop input is zero.

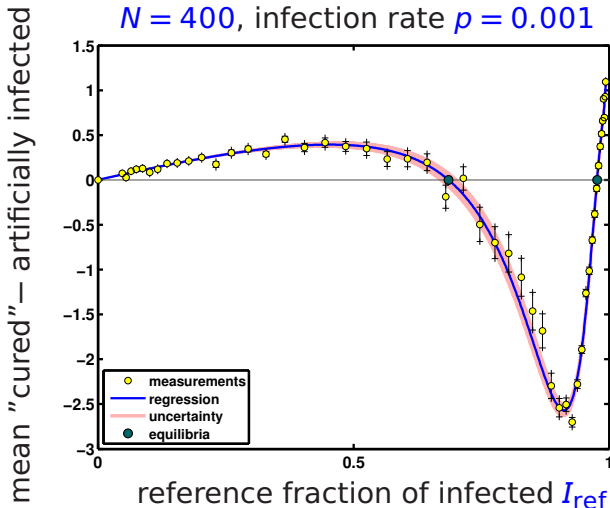
$$\lim_{t \rightarrow \infty} E[I(t) - I_{\text{ref}}] = 0$$

- ▶ For large N : $\lim_{t \rightarrow \infty} E[I(t) - I_{\text{ref}}]^2 \sim N^{-1}$.
- ▶ Resulting equilibrium I_{ref} independent of choice of feedback loop for $N \rightarrow \infty$.

Proposed definition of (unstable) equilibrium

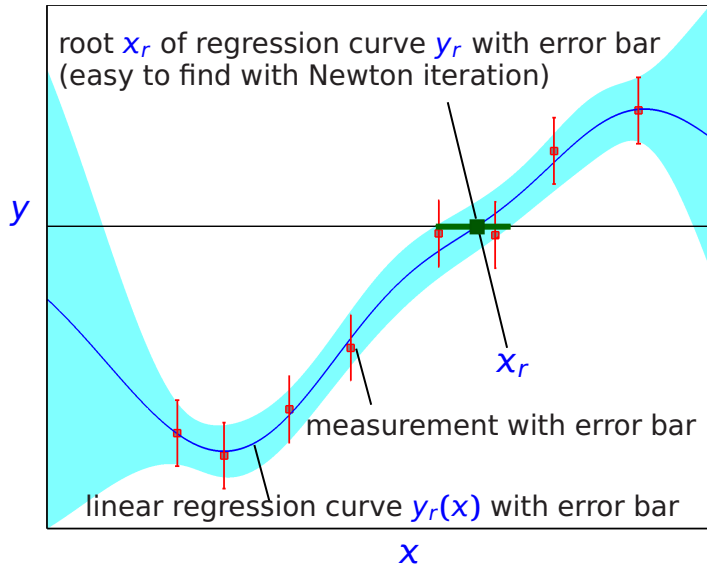
mean control input & regression curve

$N = 400$, infection rate $p = 0.001$



Newton iteration & continuation with uncertainty

Linear regression with Gaussian process



Procedure for continuation with uncertainty

Inner loop (replacing Newton iteration):

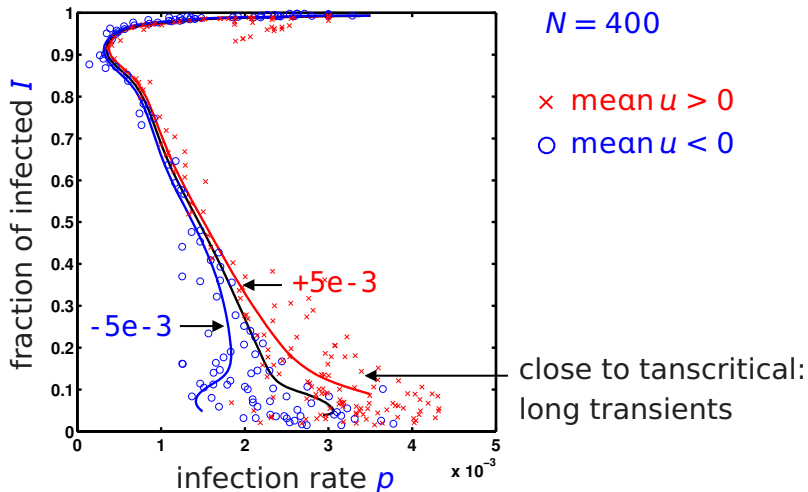
1. find root x_0 of regression curve $y_r(x)$ with Newton it.
2. determine where to measure next:
 - ▶ x for which measurement $y_r(x) \pm \sigma_r(x)$ would minimize error bar of root x_0 for updated y_r , or
 - ▶ x where measurement $y_r(x) \pm \sigma_r(x)$ changes root x_0 the most

Both are nonlinear optimization problems on current regression curve y_r (cheap in principle).

optimal new x not necessary, only sensible x

3. stop if expected effect on root x_0 is not worth additional measurement.
4. measure (mean y , var y) at new x , update (y_r, σ_r) with new value
5. back to 1.

Disease on network equilibrium continuation



Disease on network equilibrium continuation

Animation of fold continuation

Continuation in experiments

- ▶ evaluation of residual $F : (y_{\text{ref}}, p) \rightarrow y_{\infty}$ is slow
- ⇒ restricted to low dimension of control inputs and small number of (eg) Fourier modes
- ▶ low accuracy of F (relative error $\approx 10^{-2}$ in clean experiments)
- ⇒ restricted to well-conditioned problems
- ⇒ F. Schilder's `coco` toolbox `continex`
- ▶ limiting factor: ability to provide stabilizing real-time feedback
- ⇒ hardest part is problem specific
- ⇒ new algorithms needed